OOFEM Element Library Manual

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Contents

In	oduction
E	ments for Structural Analysis (SM Module)
2.	Truss Elements
	2.1.1 Truss 1D element
	2.1.2 Truss 2D element
	2.1.3 Truss 3D element
2.	Beam Elements
	2.2.1 Beam2d element
	2.2.2 Beam3d element
2.	LatticeElements
	2.3.1 Lattice2d
2.	Plane Stress Elements
	2.4.1 PlaneStress2d
	2.4.2 OPlaneStress2d
	2 4 3 TrPlaneStress2d
	244 OTrPlStr
	2.4.5 TrPlaneStrBot
	2.4.5 TrPlaneStrassBot Allman
2	Plane Strain Flomonts
2.	2.5.1 Quad1DlanoStrain
	$2.9.1$ Guadifi and Strain $\dots \dots \dots$
2	2.0.2 Inplate Strall
Δ.	Plate & Sheh Elements
	2.0.1 DK1 Element
	2.6.2 QDK1 Element
	2.6.3 CCT Element
	2.6.4 CC13D Element
	2.6.5 RerShell Element
	2.6.6 tr_shell01 element
	2.6.7 tr_shell02 element
	2.6.8 Quad1Mindlin Element
	2.6.9 Tr2Shell7 Element
	2.6.10 MITC4Shell Element
	2.6.11 Sub-soil Elements
	2.6.12 quad1plateSubsoil Element
	2.6.13 Tria1PlateSubSoil Element
2.	Axisymmetric Elements
	2.7.1 Axisymm3d element
	2.7.2 Q4axisymm element
	2.7.3 L4axisymm element
2.	3d Continuum Elements
	2.8.1 LSpace element
	2.8.2 LSpaceBB element
	2.8.3 QSpace element
	2.8.4 LTRSpace element
	2.8.5 QTRSpace element
	2.8.6 LWedge element
	2.8.7 QWedge element
2.	Interface elements
_,	2.9.1 IntElPoint. Interface1d elements
	2.9.2 IntElLine1. Interface2dlin elements
	2.9.3 IntElLine2. Interface2douad elements
	2.9.4 IntElSurfTr1 Interface3dtrlin elements
2	Free warning analysis elements

		2.10.1 TrWarp	40
	2.11	XFEM elements	41
		2.11.1 TrPlaneStress2dXFEM element	41
		2.11.2 PlaneStress2dXfem element	41
	2.12	Iso Geometric Analysis based (IGA) elements	43
	2.13	Special elements	44
		2.13.1 LumpedMass element	44
		2.13.2 Spring element	44
	2.14	Geometric nonlinear analysis	46
			-
3	Eler	nents for Transport problems (TM Module)	47
	3.1	2D Elements	47
		3.1.1 Tr1ht element	47
		3.1.2 Tr1mt element	47
		3.1.3 Tr1hmt element	47
		3.1.4 Quad1ht element	48
		3.1.5 Quad1mt element	48
		3.1.6 Quad1hmt element	48
	3.2	Axisymmetric Elements	49
		3.2.1 Quadaxisym1ht element	49
		3.2.2 Traxisym1ht element	49
	3.3	3D Elements	50
		3.3.1 Tetrah1ht - tetrahedral 3D element	50
		3.3.2 Brick1ht - hexahedral 3D element	50
		3.3.3 Brick1hmt - hexahedral 3D element	51
		3.3.4 QBrick1ht - quadratic hexahedral 3D element	51
		3.3.5 QBrick1hmt - quadratic hexahedral 3D element	51
		• 1	
4	Eler	nents for Fluid Dynamics problems (FM Module)	53
	4.1	Stokes' Flow Elements	53
		4.1.1 Tr21Stokes element	53
		4.1.2 Tet21Stokes element	53
		4.1.3 Hexa21Stokes element	53
		4.1.4 Tr1BubbleStokes element	54
		4.1.5 Tet1BubbleStokes element	54
	4.2	2D CBS Elements	56
		4.2.1 Tr1CBS element	56
	4.3	2D SUPG/PSGP Elements	57
		4.3.1 Tr1SUPG element	57
		4.3.2 Tr21SUPG element	57
		4.3.3 Tr1SUPGAxi element	58
	4.4	3D SUPG/PSGP Elements	60
		4.4.1 Tet1_3D_SUPG element	60

List of Figures

1	Truss2d element in (x,z) plane	3	
2	Beam2d element. Definition of local c.s.(a) and definition of local end forces and local element		
	dofs (b)	5	
3	Beam3d element. Definition of local c.s., local end forces and local element dofs numbering	6	
4	Lattice2d element. Node numbering, DOF numbering and definition of integration point C	8	
5	PlaneStress2d element. Node numbering, edge numbering and definition of local edge c.s.(a).	9	
6	QPlaneStress2d element - node numbering.	10	
7	TrPlaneStress2d element - node and side numbering	11	
8	QTrPlStr element - node and side numbering	11	
9	Quad1PlaneStrain element. Node numbering, Side numbering and definition of local edge c.s.(a).	16	
10	TrplaneStrain element - node and side numbering.	17	
11	Geometry of tr_shell01 element.	20	
12	LSpace element (Node numbers in black, side numbers in blue, and surface numbers in red)	31	
13	QSpace element.	32	
14	LTRSpace element. Definition and node numbering convention	33	
15	QTRSpace element. Definition and node numbering convention	33	
16	LWedge element. Node numbering convention in black, edge numbering in blue and face		
	numbering in red	34	
17	QWedge element. Node numbering convention in black, edge numbering in blue and face		
	numbering in red	34	
18	Interface2dlin element with linear interpolation. Definition and node numbering convention	37	
19	Interface2dquad element with quadratic interpolation. Definition and node numbering convention	38	
20	Interface3dtrlin element with linear interpolation. Definition and node numbering convention .	39	
21	Tr1ht element - node and side numbering.	47	
22	Quad1ht element. Node numbering, Side numbering and definition of local edge c.s.(a).	48	
23	Brick1ht element. Node numbers are in black, side numbers are in blue, and surface numbers	-	
~ .	are in red	50	
24	Hexa21Stokes element. Node numbering and face numbering	54	
25	TrICBS element. Node numbering, Side numbering and definition of local edge c.s.(a)	56	
26	TrISUPG element. Node numbering, Side numbering and definition of local edge c.s.(a)	57	
27	Tr21SUPG element - node and side numbering.	58	
28	TrISUPGAxi element. Node numbering, Side numbering and definition of local edge c.s.(a)	59	
29	Tet1_3D_SUPG element.	60	

1 Introduction

In this manual the detailed description of available elements is given. The actual availability of particular elements depends on OOFEM configuration. Elements are specified using element records, which are part of oofem input file. The general format of element record is described in OOFEM input manual.

Every element is described in a separate section. The section includes the "element keyword", which determines the element type in element record, approximation and interpolation characteristics, required cross section properties (which are summarized in "CS properties" part), and a summary of element features. The "Load" section contains useful information about the types of loadings supported by particular elements.

2 Elements for Structural Analysis (SM Module)

2.1 Truss Elements

2.1.1 Truss 1D element

Represents linear isoparametric truss element in 1D. The elements are assumed to be located along the x-axis. Requires cross section area to be specified. The element features are summarized in Table 1.

Keyword	truss1d
Description	1D truss element
Specific parameters	-
Unknowns	Single dof (u-displacement) is required in each node
Approximation	Linear approximation of displacement and geometry
Integration	Exact
Features	Full dynamic analysis support, Full nonlocal constitutive
	support, Adaptivity support
CS properties	Area is required
Loads	Body loads are supported. Boundary loads are not sup-
	ported in current implementation
Status	Reliable

Table 1: truss1d element summary

2.1.2 Truss 2D element

Two node linear isoparametric truss element for 2D analysis. The element geometry can be specified in (x,z), (x,y), or (y,z) plane. The element features are summarized in Table 2.



Figure 1: Truss2d element in (x,z) plane.

Keyword	m truss2d
Description	2D truss element
Specific parameters	$[cs \#_{(in)}]$
Parameters	cs: this parameter can be used to change default definition
	plane. The supported values of cs are following: 0 for (x,z)
	plane (default), 1 for (x,y) plane, and 3 for (y,z) plane.
Unknowns	Two dofs representing displacements in definition plane are
	required in each node. The element can be used in different
	planes, default definition plane is (x,z) . The parameter cs
	can be used to change default definition plane.
Approximation	Linear approximation of displacements and geometry.
Integration	Exact.
Features	Full dynamic analysis support. Full nonlocal constitutive
	support.
CS properties	cross section area should be provided.
Loads	Edge loads are supported, Edge number should be equal to
	1
Status	Reliable

Table 2: truss2d element summary

truss2d element summarytruss2dsummary

2.1.3 Truss 3D element

Two node linear isoparametric truss element for 3D analysis. The element geometry is specified in (x,y,z) plane. The element features are summarized in Table 3.

Keyword	truss3d
Description	3D truss element
Specific parameters	-
Unknowns	Three displacement DOFs (in x, y, and z directions) are
	required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Exact.
Features	Full dynamic analysis support. Full nonlocal constitutive
	support.
CS properties	cross section area should be provided.
Status	Reliable

Table 3: truss3d element summary

2.2 Beam Elements

2.2.1 Beam2d element

Beam element for 2D analysis, based on Timoshenko hypothesis. Structure should be defined in x,z plane. The internal condensation of arbitrary DOF is supported and is performed in local coordinate system. On output, the local end displacement and local end forces are printed. The element features are summarized in Table 4.



Figure 2: Beam2d element. Definition of local c.s.(a) and definition of local end forces and local element dofs (b).

Keyword	beam2d
Description	2D beam element
Specific parameters	$[\texttt{dofstocondense} \ \#_{(ia)}]$
Parameters	dofstocondense: allows to specify local element dofs that will be condensed. The numbering of local element dofs is shown in fig. 2. The size of this array should be equal to number of local element dofs (6) and nonzero value indicates
TT 1	the corresponding dof will be condensed.
Unknowns	required in each node.
Approximation	Cubic approximations of lateral displacement and rotation are used. For longitudinal displacement the linear one is assumed.
Integration	Exact.
Features	Full dynamic analysis support. Linear stability analysis support.
CS properties	Area, inertia moment along y-axis (iy parameter) and equiva- lent shear area (shearareaz parameter) should be specified.
Loads	Constant and linear edge loads are supported, shear influ- ence is taken into account. Edge number should be equal to 1. Temperature load is supported, the first coefficient of temperature load represent mid-plane temperature change, the second one represent difference between temperature change of local z + and local z - surfaces of beam (in local co- ordinate system). Temperature load require that the "thick" property of cross section model is defined.
Status	Reliable

Table 4: beam2d element summary

2.2.2 Beam3d element

Beam element for 3D **linear** analysis, based on Timoshenko hypothesis. The internal condensation of arbitrary DOF is supported and is performed in local coordinate system. On output, the local end-displacement and local end-forces are printed. Requires the local coordinate system to be chosen according to main central axes of inertia. Local element coordinate system is determined by the following rules:

- 1. let first element node has following coordinates (x_i, y_i, z_i) and the second one (x_j, y_j, z_j) ,
- 2. direction vector of local x-axis is then $\mathbf{a}_1 = (x_j x_i, y_j y_i, z_j z_i),$
- 3. local y-axis direction vector lies in plane defined by local x-axis direction vector (\mathbf{a}_1) and given point (k-node with coordinates (x_k, y_k, z_k)) so called reference node,
- 4. local z-axis is then determined as vector product of local x-axis direction vector (\mathbf{a}_1) by vector $(x_k x_i, y_k y_i, z_k z_i)$,
- 5. local y-axis is then determined as vector product of local z-axis direction vector by local x-axis direction vector.

The element features are summarized in Table 5.



Figure 3: Beam3d element. Definition of local c.s., local end forces and local element dofs numbering.

Keyword	beam3d
Description	3D beam element
Specific parameters	refnode $\#_{(in)}$ [dofstocondense $\#_{(ia)}$]
Parameters	refnode: sets reference node to determine the local coordi-
	nate system of element.
	dofstocondense: allows to specify local element dofs that
	will be condensed. The numbering of local element dofs
	is shown in fig. 3. The size of this array should be equal
	to number of local element dofs (12) and nonzero value
	indicates the corresponding dof will be condensed.
Unknowns	Six dofs (u,v,w-displacements and x,y,z-rotations) are re-
	quired in each node.
Approximation	Cubic approximations of lateral displacement and rotation
	(along local y,z axes) are used. For longitudinal displace-
	ment and the rotation along local x-axis (torsion) the linear
	approximations are assumed.
Integration	Exact.
Features	Full dynamic analysis support. Linear stability analysis
aa	support.
CS properties	Area, inertia moment along y and z axis (1y and 1z param-
	eters), torsion inertia moment (ik parameter) and either
	cross section area snear correction factor (beamsnear coeff
	parameter) of equivalent shear areas (shear areas and
	properties are assumed to be defined in least coordinate
	system of element
Loads	Constant and linear edge loads are supported. Edge number
LUaus	should be equal to 1. Temperature load is supported, the
	first coefficient of temperature load represent mid-plane
	temperature change the second one represent difference
	between temperature change of local z + surface and local z -
	surface surface of beam and the third one represent difference
	between temperature change of local v+ surface and local v-
	surface of beam. Requires the "thick" (measured in direction
	of local z axis) and "width" (measured in direction of local
	y axis) cross section model properties to be defined.
Status	Reliable

Table 5: beam3d element summary

2.3 LatticeElements

2.3.1 Lattice2d

Represents two-node lattice element. Each node has 3 degrees of freedom. The element is defined in x,y plane. The element features are summarized in Table 6.



Figure 4: Lattice2d element. Node numbering, DOF numbering and definition of integration point C.

Keyword	lattice2d
Description	Lattice element
Specific parameters	thick $\#_{(\mathrm{rn})}$ width $\#_{(\mathrm{rn})}$ gpCoords $\#_{(\mathrm{ra})}$
Parameters	thick: defines the out of plane $(z$ -direction) thickness
	width: defines the width of the midpoint cross-section in
	the $x-y$ plane with the point C at its centre
	gpCooords: array of the coordinates of the integration point
	C in the global coordinate system
Unknowns	Three dofs (u -displacement, v -displacement, w -rotation) are
	required in each node.

Table 6: lattice2d element summary

2.4 Plane Stress Elements

2.4.1 PlaneStress2d

Represents isoparametric four-node quadrilateral plane-stress finite element. Each node has 2 degrees of freedom. Structure should be defined in x,y plane. The nodes should be numbered anti-clockwise (positive rotation around z-axis). The element features are summarized in Table 7.

The generalization of this element, that can be positioned arbitrarily in space is linquad3dplanestress element. This element requires 3 displacement degrees of freedon in each node and assumes, that the element geometry is flat, i.e. all nodes are in the same plane. The element features are summarized in Table 8.



Figure 5: PlaneStress2d element. Node numbering, edge numbering and definition of local edge c.s.(a).

Keyword	planestress2d
Description	2D quadrilateral element for plane stress analysis
Specific parameters	$[\text{NIP } \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using Gauss integra-
	tion formula in 1, 4 (default), 9 or 16 integration points. The
	default number of integration points used can be overloaded
	using NIP parameter. Reduced integration for shear terms
	is employed. Shear terms are always integrated using the
	1-point integration rule.
Features	Nonlocal constitutive support, Geometric nonlinearity sup-
	port.
CS properties	cross section thickness is required.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side num-
	bering is following. Each i-th element side begins in i-th
	element node and ends on next element node (i+1-th node
	or 1-st node, in the case of side number 4). The local posi-
	tive edge x-axis coincides with side direction, the positive
	local edge y-axis is rotated 90 degrees anti-clockwise (see
	fig. (5)).
Nlgeo	0, 1.
Status	Reliable

Table 7: planestress2d element summary

Keyword	linguad3dplanestress
Description	3D quadrilateral element for plane stress analysis
Specific parameters	[NIP #(in)]
Parameters	NIP: allows to set the number of integration points
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using Gauss integra-
	tion formula in 1, 4 (default), 9 or 16 integration points. The
	default number of integration points used can be overloaded
	using NIP parameter. Reduced integration for shear terms
	is employed. Shear terms are always integrated using the
	1-point integration rule.
Features	Nonlocal constitutive support, Geometric nonlinearity sup-
	port.
CS properties	cross section thickness is required.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side num-
	bering is following. Each i-th element side begins in i-th
	element node and ends on next element node (i+1-th node
	or 1-st node, in the case of side number 4). The local posi-
	tive edge x-axis coincides with side direction, the positive
	local edge y-axis is rotated 90 degrees anti-clockwise (see
	fig. (5)).
Nlgeo	0, 1.
Status	Basic functionality tested, element loads need further test-
	ing.

Table 8: linquad3dplanestress element summary

2.4.2 QPlaneStress2d

Implementation of quadratic isoparametric eight-node quadrilateral plane-stress finite element. Each node has 2 degrees of freedom. The node numbering is anti-clockwise and is explained in fig. (6). The element features are summarized in Table 9.



Figure 6: QPlaneStress2d element - node numbering.

2.4.3 TrPlaneStress2d

Implements an triangular three-node constant strain plane-stress finite element. Each node has 2 degrees of freedom. The node numbering is anti-clockwise. The element features are summarized in Table 10.

Keyword	${ m qplanestress2d}$
Description	2D quadratic isoparametric plane stress element
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Quadratic approximation of displacements and geometry.
Integration	Full integration using Gauss integration formula in 4 (the
	default), 9 or 16 integration points. The default number
	of integration points used can be overloaded using NIP
	parameter.
Features	Adaptivity support.
CS properties	Cross section thickness is required.
Loads	Body and boundary loads are supported.
Nlgeo	0, 1.
Status	Stable

Table 9: qplanestress2d element summary



Figure 7: TrPlaneStress2d element - node and side numbering.

Keyword	trplanestress2d
Description	2D linear triangular isoparametric plane stress element
Specific parameters	-
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using one point gauss integration formula.
Features	Nonlocal constitutive support, Edge load support, Geomet-
	ric nonlinearity support, Adaptivity support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported. Boundary loads are supported
	and are computed using numerical integration. The side
	numbering is following. Each i-th element side begins in i-th
	element node and ends on next element node (i+1-th node or
	1-st node, in the case of side number 3). The local positive
	edge x-axis coincides with side direction, the positive local
	edge y-axis is rotated 90 degrees anti-clockwise (see fig. (7)).
Nlgeo	0, 1.
Status	Reliable

Table 10: trplanestress2d elemen	t summary
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2.4.4 QTrPlStr

Implementation of quadratic six-node plane-stress finite element. Each node has 2 degrees of freedom. Node numbering is anti-clockwise and is shown in fig. (8). The element features are summarized in Table 11.



Figure 8: QTrPlStr element - node and side numbering.

Keyword	qtrplstr
Description	2D quadratic triangular plane stress element
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Quadratic approximation of displacements and geometry.
Integration	Full integration using gauss integration formula in 4 points
	(the default) or in 7 points (using NIP parameter).
Features	Adaptivity support (error indicator).
CS properties	Cross section thickness is required.
Loads	Boundary loads are supported.
Nlgeo	0, 1.
Status	-

Table 11: qtrplstr element summary

2.4.5 TrPlaneStrRot

Implementation of triangular three-node plane-stress finite element with independent rotation field. Each node has 3 degrees of freedom. The element features are summarized in Table 12.

The generalization of this element, that can be positioned arbitrarily in space is trplanestrrot3d element. This element requires 6 degrees of freedon in each node. The element features are summarized in Table 13.

The implementation is based on the following paper: Ibrahimbegovic, A., Taylor, R.L., Wilson, E. L.: A robust membrane qudritelar element with rotational degrees of freedom, Int. J. Num. Meth. Engng., 30, 445-457, 1990. The rotation field is defined as $\omega = \frac{1}{2} \left(\frac{dv}{dx} - \frac{du}{dy} \right) = \nabla_u \boldsymbol{u}$. The following form of potential energy functial is assumed:

$$\Pi = \frac{1}{2} \int_{\Omega} \boldsymbol{\sigma}^{T} \boldsymbol{\varepsilon} \ d\Omega + \int_{\Omega} \boldsymbol{\tau}^{T} (\nabla_{\boldsymbol{u}} \boldsymbol{u} - \boldsymbol{\omega}) \ d\Omega - \int_{\Omega} \boldsymbol{X}^{T} \boldsymbol{u} \ d\Omega$$

where $\boldsymbol{\tau}$ is pseudo-stress (component of anti-symmetric stress tensor) working on dislocation $(\nabla_u \boldsymbol{u} - \omega)$; the following constitutive relation forms assumed: $\boldsymbol{\tau} = G(\nabla_u \boldsymbol{u} - \omega)$, where G is elasticity modulus in shear.

Keyword	trplanestrrot
Description	2D linear triangular plane stress element with rotational
	DOFs
Specific parameters	$[$ [NIP $\#_{(in)}]$ [NIPRot $\#_{(in)}]$
Parameters	NIP: allows to set the number of integration points for inte-
	gration of membrane terms.
	NIPRot: allows to set the number of integration points for
	integration of terms associated to rotational field.
Unknowns	Three dofs (u-displacement, v-displacement, z-rotation) are
	required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using gauss integration
	formula in 4 points (default) or using 1 or 7 points (using NIP
	parameter). Integration of strains associated with rotational
	field integration using 1 point is default (4 and 7 points
	rules can be specified using NIPRot parameter).
Features	-
CS properties	Cross section thickness is required.
Loads	-
Nlgeo	0.
Status	-

Table 12: trplanestrrot element summary

Keyword	trplanestrrot3d
Description	3D linear triangular plane stress element with rotational
	DOFs
Specific parameters	$[\texttt{NIP} \ \#_{(\texttt{in})}] \ [\texttt{NIPRot} \ \#_{(\texttt{in})}]$
Parameters	NIP: allows to set the number of integration points for inte-
	gration of membrane terms.
	NIPRot: allows to set the number of integration points for
	integration of terms associated to rotational field.
Unknowns	Six dofs (u-displacement, v-displacement, w-displacement,
	x-rotation, y-rotation, z-rotation) are required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using gauss integration
	formula in 4 points (default) or using 1 or 7 points (using NIP
	parameter). Integration of strains associated with rotational
	field integration using 1 point is default (4 and 7 points
	rules can be specified using NIPRot parameter).
Features	-
CS properties	Cross section thickness is required.
Loads	-
Nlgeo	0.
Status	-

Table 13: trplanestrrot3d element summary

2.4.6 TrPlaneStressRotAllman

Implementation of triangular three-node plane-stress with nodal rotations. Each node has 3 degrees of freedom. The element features are summarized in Table 14.

The generalization of this element, that can be positioned arbitrarily in space is trplanestressrotallman3d element. This element requires 6 degrees of freedon in each node. The element features are summarized in

Table 15.

The implementation is based on the following paper: Allman, D.J.: A compatible triangular element including vertex rotations for plane elasticity analysis, Computers & Structures, vol. 19, no. 1-2, pp. 1-8, 1984. The element is based on plane stress element with quadratic interpolation. The displacements in midside nodes are expressed using vertex displacements and vertex rotations (for edge normal displacement component); the tangential component is interpolated from vertex values. For particular element side starting at i-th vertex and ending in j-th vertex the normal and tangential displacements at edge midpoint can be expressed as

$$u_{n}|_{l/2} = \frac{u_{ni} + u_{nj}}{2} + \frac{l}{8}(\omega_{i} - \omega_{j})$$
$$u_{t}|_{l/2} = \frac{u_{ti} + u_{tj}}{2}$$

where l is edge length. This allows to express global displacements in element midside nodes using vertex displacements and rotations. For a single edge, one obtains:

$$\begin{aligned} u|_{l/2} &= -\frac{u_{ni} + u_{nj}}{2} + \frac{l}{8}(\omega_i - \omega_j)\frac{\Delta y_{ji}}{l} + (\frac{u_{t1} + u_{t2}}{2})\frac{\Delta x_{ji}}{l} \\ v|_{l/2} &= \frac{u_{ni} + u_{nj}}{2} + \frac{l}{8}(\omega_i - \omega_j)\frac{\Delta x_{ji}}{l} + (\frac{u_{t1} + u_{t2}}{2})\frac{\Delta y_{ji}}{l} \end{aligned}$$

Keyword	trplanestressrotallman
Description	2D linear triangular plane stress element with rotational
	DOFs
Specific parameters	
Unknowns	Three dofs (u-displacement, v-displacement, z-rotation) are
	required in each node.
Approximation	Linear approximation of geometry, quadratic interpolation
	of displacements.
Integration	Integration of membrane strain terms using gauss integration
	formula in 4 points.
Zero energy mode	The zero energy mode (equal rotations) is handled by adding
	additional energy term preventing spurious modes.
Features	-
CS properties	Cross section thickness is required.
Loads	-
Nlgeo	0.
Status	-

Table 14: trplanestressrotallman element summary

Keyword	trplanestressrotallman3d
Description	2D linear triangular plane stress element with rotational
	DOFs
Specific parameters	
Unknowns	Six dofs (D_u, D_v, D_w, R_x, R_y, R_z) are required in each
	node.
Approximation	Linear approximation of geometry, quadratic interpolation
	of displacements.
Integration	Integration of membrane strain terms using gauss integration
	formula in 4 points.
Zero energy mode	The zero energy mode (equal rotations) is handled by adding
	additional energy term preventing spurious modes.
Features	-
CS properties	Cross section thickness is required.
Loads	-
Nlgeo	0.
Status	-

Table 15: trplanestressrotallman3d element summary

2.5 Plane Strain Elements

2.5.1 Quad1PlaneStrain

Represents isoparametric four-node quadrilateral plane-strain finite element. Each node has 2 degrees of freedom. Structure should be defined in x,y plane. The nodes should be numbered anti-clockwise (positive rotation around z-axis). The element features are summarized in Table 16.



Figure 9: Quad1PlaneStrain element. Node numbering, Side numbering and definition of local edge c.s.(a).

Keyword	quad1planestrain
Description	2D linear quadrilateral plane-strain element
Specific parameters	$[\texttt{NIP} \ \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points for inte-
	gration of membrane terms.
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using gauss integration
	formula in 4 (the default), 9 or 16 integration points. The
	default number of integration points used can be overloaded
	using NIP parameter. Reduced integration for shear terms is
	employed. Shear terms are always integrated using 1 point
	integration rule.
Features	Nonlocal constitutive support, Adaptivity support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side num-
	bering is following. Each i-th element side begins in i-th
	element node and ends on next element node (1+1-th node
	or 1-st node, in the case of side number 4). The local posi-
	tive edge x-axis collicides with side direction, the positive
	local edge y-axis is rotated 90 degrees anti-clockwise (see f_{π} (0))
Nlgoo	ng. (9)).
Status	u. Reliable
Status	Reliable

Table 16: quad1planestrain element summary

2.5.2 TrplaneStrain

Implements an triangular three-node constant strain plane-strain finite element. Each node has 2 degrees of freedom. The node numbering is anti-clockwise. The element features are summarized in Table 17.



Figure 10: TrplaneStrain element - node and side numbering.

Keyword	trplanestrain
Description	2D linear triangular plane-strain element
Specific parameters	-
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration of membrane strain terms using one point gauss integration formula.
Features	Nonlocal constitutive support. Edge load support, Adaptiv- ity support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported. Boundary loads are supported and are computed using numerical integration. The side numbering is following. Each i-th element side begins in i-th element node and ends on next element node (i+1-th node or 1-st node, in the case of side number 3). The local positive edge x-axis coincides with side direction, the positive local edge y-axis is rotated 90 degrees anti-clockwise (see fig. (10)).
Nlgeo	0.
Status	Reliable

Table 17: trplanestrain element summary

2.6 Plate & Shell Elements

2.6.1 DKT Element

Implementation of Discrete Kirchhoff Triangle (DKT) plate element. This element is suitable for thin plates, as the traswerse shear strain energy is neglected. The structure should be defined in x,y plane, nodes should be numbered anti-clockwise (positive rotation around z-axis). The element features are summarized in Table 18.

Keyword	dktplate
Description	2D Discrete Kirchhoff Triangular plate element
Specific parameters	-
Unknowns	Three dofs (w-displacement, u and v - rotations) are required
	in each node.
Approximation	Quadratic approximation of rotations, cubic approximation
	of displacement along the edges. Note: there is no need to
	define interpolation for displacement on the element.
Integration	Default integration of all terms using three point formula.
Features	Layered cross section support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported. Boundary load support is beta.
Output	On output, the generalized shell strain/force momentum
	vectors in global coordinate system are printed, with the
	following meaning:
	$s_{\varepsilon} = \{\varepsilon_x, \varepsilon_y, \varepsilon_{xz}, \kappa_x, \kappa_y, \kappa_{xy}, \gamma_{xz}, \gamma_{yz}\},\$
	$s_{\sigma} = \{n_x, n_y, n_{xy}, m_x, m_y, m_z, m_{xy}, q_{xz}, q_{yz}\}$
	where $\varepsilon_x, \varepsilon_y, \varepsilon_{xy}$ are membrane in plane normal deforma- tions, γ_{zx}, γ_{xz} are (out of plane and in plane) shear com-
	ponets, $\kappa_x, \kappa_y, \kappa_{xy}$ are curvatures, $n_x, n_y, n_{xy}, q_{xz}, q_{yz}$ are integral forces (normal and shear forces), and m_x, m_y, m_{xy} are bending moments. Please note, for example, that bend- ing moment m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along the y-axis and positive value causes tension in bottom layer.
Nlgeo	0.
Status	Reliable
Reference	J.L.Batoz, K.J.Bathe, L.W.Ho: A study of three-node tri-
	angular plate bending elements, IJNME, 15(12):1771-1812, 1980

Table 18: DKTplate element summary

2.6.2 QDKT Element

Implementation of Discrete Kirchhoff Theory plate quad element (QDKT). This element is suitable for thin plates, as the traswerse shear strain energy is neglected. The structure should be defined in x,y plane, nodes should be numbered anti-clockwise (positive rotation around z-axis). The element features are summarized in Table 19.

2.6.3 CCT Element

Implementation of constant curvature triangular element for plate analysis. Formulation based on Mindlin hypothesis. The structure should be defined in x,y plane. The nodes should be numbered anti-clockwise

Keyword	qdktplate
Description	2D Discrete Kirchhoff Quad plate element
Specific parameters	-
Unknowns	Three dofs (w-displacement, u and v - rotations) are required
	in each node.
Approximation	Quadratic approximation of rotations, cubic approximation
	of displacement along the edges. Note: there is no need to
	define interpolation for displacement on the element.
Integration	Default integration of all bending terms using four point
	formula.
Features	Layered cross section support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported.
Output	On output, the generalized shell strain/force momentum
	vectors in global coordinate system are printed, with the
	following meaning:
	$e - \{e e e \kappa \kappa \kappa \gamma \gamma \}$
	$s_{\varepsilon} = \{\varepsilon_x, \varepsilon_y, \varepsilon_{xz}, \kappa_x, \kappa_y, \kappa_{xy}, xz, yz\}, $
	$s_{\sigma} = \{n_x, n_y, n_{xy}, m_x, m_y, m_z, m_{xy}, q_{xz}, q_{yz}\}$
	where $\varepsilon_x, \varepsilon_y, \varepsilon_{xy}$ are membrane in plane normal deforma-
	tions, γ_{zx}, γ_{xz} are (out of plane and in plane) shear com-
	ponets, $\kappa_x, \kappa_y, \kappa_{xy}$ are curvatures, $n_x, n_y, n_{xy}, q_{xz}, q_{yz}$ are
	integral forces (normal and shear forces), and m_x, m_y, m_{xy}
	are bending moments. Please note, for example, that bend-
	ing moment m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along
	the y-axis and positive value causes tension in bottom layer.
Nlgeo	0.
Status	Reliable
Reference	J.L.Batoz, K.J.Bathe, L.W.Ho: A study of three-node tri-
	angular plate bending elements, IJNME, 15(12):1771-1812,
	1980

Table 19: QDKTplate element summary

(positive rotation around z-axis). The element features are summarized in Table 20.

2.6.4 CCT3D Element

Implementation of constant curvature triangular element for plate analysis. Formulation based on Mindlin hypothesis. The element could be arbitrarily oriented in space. The nodes should be numbered anti-clockwise (positive rotation around element normal). The element features are summarized in Table 21.

2.6.5 RerShell Element

Combination of CCT plate element (Mindlin hypothesis) with triangular plane stress element for membrane behavior. The element curvature can be specified. Although element requires generally six DOFs per node, no stiffness to local rotation along z-axis (rotation around element normal) is supplied. The element features are summarized in Table 22.

Keyword	cctplate
Description	2D constant curvature triangular plate element
Specific parameters	-
Unknowns	Three dofs (w-displacement, u and v - rotations) are required
	in each node.
Approximation	Linear approximation of rotations, quadratic approximation
	of displacement.
Integration	Integration of all terms using one point formula.
Features	Layered cross section support.
CS properties	Cross section thickness is required.
Loads	Body loads are supported. Boundary loads are not sup-
	ported now.
Output	On output, the generalized shell strain/force momentum
	vectors in global coordinate system are printed, with the
	following meaning:
	$s_{\varepsilon} = \{\varepsilon_x, \varepsilon_y, \varepsilon_{xz}, \kappa_x, \kappa_y, \kappa_{xy}, \gamma_{xz}, \gamma_{yz}\},\$
	$s_{\sigma} = \{n_x, n_y, n_{xy}, m_x, m_y, m_z, m_{xy}, q_{xz}, q_{yz}\}$
	where $\varepsilon_x, \varepsilon_y, \varepsilon_{xy}$ are membrane in plane normal deforma- tions, γ_{zx}, γ_{xz} are (out of plane and in plane) shear com- ponets, $\kappa_x, \kappa_y, \kappa_{xy}$ are curvatures, $n_x, n_y, n_{xy}, q_{xz}, q_{yz}$ are integral forces (normal and shear forces), and m_x, m_y, m_{xy} are bending moments. Please note, for example, that bend- ing moment m_x is defined as $m_x = \int \sigma_{xz} dz$, so it acts along the y-axis and positive value causes tension in bottom layer.
Nlgeo	0.
Status	Reliable

Table 20: cctplate element summary

2.6.6 tr_shell01 element

Combination of CCT3D plate element (Mindlin hypothesis) with triangular plane stress element for membrane behavior. It comes with complete set of 6 DOFs per node. The element features are summarized in Table 23.



Figure 11: Geometry of tr_shell01 element.

Keyword	cctplate3d	
Description	Constant curvature triangular plate element in arbitray	
	position	
Specific parameters	-	
Unknowns	Six dofs (u,v,w-displacements and u,v,w rotations) are in	
	general required in each node.	
Approximation	Linear approximation of ratations, quadratic approximation	
	of displacement.	
Integration	Integration of all terms using one point formula.	
Features	Layered cross section support.	
CS properties	Cross section thickness is required.	
Loads	Body loads are supported. Boundary loads are not supported now.	
Output	On output, the shell force (s_f) , shell strain (s_s) , shell mo-	
	mentum (s_m) , and shell curvature (s_c) tensors in global	
	coordinate system are printed as vector form with 6 compo-	
	nents, with the following meaning:	
	$s_f = \{n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}\},\$	
	$s_s = \{\varepsilon_x, \varepsilon_y, \varepsilon_z, \gamma_{yz}, \gamma_{xz}, \gamma_{xy}\},\$	
	$s_m = \{m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}\},\$	
	$s_c = \{\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}\}$	
	where $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are membrane normal deformations,	
	$\gamma_{zy}, \gamma_{zx}, \gamma_{xy}$ are (out of plane and in plane) shear	
	componets, $\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}$ are curvatures,	
	$n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}$ are integral forces (normal and	
	shear forces), and $m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}$ are bending	
	moments. Please note, for example, that bending moment	
	m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along the y-axis	
	and positive value causes tension in bottom layer.	
Nigeo	0. D. 11. 11.	
Status	Rehable	

Table 21: cctplate3d element summary

2.6.7 tr_shell02 element

Combination of thin-plate DKT plate element with plane stress element (TrPlanestressRotAllman). This element comes with complete set of 6 DOFs per node. The element features are summarized in Table 24.

2.6.8 Quad1Mindlin Element

This class implements an quadrilateral, bilinear, four-node Mindlin plate. This type of element exhibit strong shear locking (thin plates exhibit almost no bending). Implements the lumped mass matrix. The element features are summarized in Table 25.

2.6.9 Tr2Shell7 Element

This class implements a triangular, quadratic, six-node shell element. The element is a so-called seven parameter shell with seven dofs per node – a displacement field (3 dofs), an extensible director field (3 dofs) and a seventh

Keyword	rershell	
Description	Simple shell based on combination of CCT plate element	
	(Mindlin hypothesis) with triangular plane stress element.	
	element can be arbitrary positioned in space.	
Specific parameters	-	
Unknowns	Six dofs (u,v,w-displacements and u,v,w rotations) are in	
	general required in each node. Note, that although element	
	it requires generally six DOFs per node, no stiffness to local	
	rotation along z-axis (rotation around element normal) is supplied.	
Approximation	Linear approximation of ratations, quadratic approximation	
II	of displacement.	
Integration	Integration of all terms using one point formula.	
Features	Layered cross section support.	
CS properties	Cross section thickness is required.	
Loads	Body loads are supported. Boundary loads are not sup-	
	ported now.	
Output	On output, the shell force (s_f) , shell strain (s_s) , shell mo-	
	mentum (s_m) , and shell curvature (s_c) tensors in global	
	coordinate system are printed as vector form with 6 com-	
	ponents, with the following meaning:	
	$s_f = \{n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}\},\$	
	$s_s = \{\varepsilon_x, \varepsilon_y, \varepsilon_z, \gamma_{yz}, \gamma_{xz}, \gamma_{xy}\},\$	
	$s_m = \{m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}\},\$	
	$s_c = \{\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}\}$	
	where $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are membrane normal deformations,	
	$\gamma_{zy}, \gamma_{zx}, \gamma_{xy}$ are (out of plane and in plane) shear	
	componets, $\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}$ are curvatures,	
	$n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}$ are integral forces (normal and	
	shear forces), and $m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}$ are bending	
	moments. Please note, for example, that bending moment	
	m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along the y-axis	
Nigoo	and positive value causes tension in bottom layer.	
Status	u. Baliabla	
l Suatus		

Table 22: rershell element summary

dof representing inhomogenous thickness strain. This last parameter is included in the model in order to deal with volumetric/Poisson lock effects.

The element features are summarized in Table 25.

2.6.10 MITC4Shell Element

A four-node quadrilateral shell element formulated using three-dimensional continuum mechanics theory degenerated to shell behaviour. The element is applicable to thick and thin shells as the "mixed interpolation of tensorial components" (MITC) approach is used to remove shear locking. The implementation is based on the following paper: Dvorkin, E.N., Bathe, K.J.: A continuum mechanics based four-node shell element for general non-linear analysis, Eng.Comput., Vol.1, 77-88, 1984.

Although element requires generally six DOFs per node, no stiffness to local rotation along z-axis (rotation around director vector) is supplied. The element features are summarized in Table 27.

Keyword	tr_shell01	
Description	Triangular shell element combining CCT3D plate element	
	(Mindlin hypothesis) with triangular plane stress element	
	with rotational DOFs	
Specific parameters	-	
Unknowns	Six dofs (u,v,w-displacements and u,v,w rotations) are in general required in each node.	
Approximation	See description of cct and trplanstrrot elements	
Integration	Integration of all terms using one point formula.	
Features	Layered cross section support.	
CS properties	Cross section thickness is required.	
Loads	Body loads are supported. Boundary loads are supported (only surface loads).	
Output	On output, the shell force (s_f) , shell strain (s_s) , shell mo- mentum (s_m) , and shell curvature (s_c) tensors in global coordinate system are printed as vector form with 6 com- ponents, with the following meaning:	
	$s_f = \{n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}\},\$	
	$s_s = \{\varepsilon_x, \varepsilon_y, \varepsilon_z, \gamma_{yz}, \gamma_{xz}, \gamma_{xy}\},\$	
	$s_m = \{m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}\},\$	
	$s_c = \{\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}\}$	
	where $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are membrane normal deformations, $\gamma_{zy}, \gamma_{zx}, \gamma_{xy}$ are (out of plane and in plane) shear componets, $\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}$ are curvatures, $n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}$ are integral forces (normal and shear forces), and $m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}$ are bending moments. Please note, for example, that bending moment m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along the y-axis and positive value causes tension in bottom layer.	
Nlgeo	0.	
Status	Reliable	

Table 23: tr_shell01 element summary

2.6.11 Sub-soil Elements

2.6.12 quad1plateSubsoil Element

This class implements an quadrilateral, bilinear, four-node plate subsoil element. Typically this element is combined with suitable plate element with quadrilateral geometry to model plate element on (elastic) subsoill foundation, but it can be used alone. The element geometry should be define in xy plane. The element features are summarized in Table 28.

2.6.13 Tria1PlateSubSoil Element

This class implements an quadrilateral, bilinear, four-node plate subsoil element. Typically this element is combined with suitable plate element with quadrilateral geometry to model plate element on (elastic) subsoill foundation, but it can be used alone. The element geometry should be define in xy plane. The element features are summarized in Table 28.

Keyword	tr_shell02	
Description	Triangular shell element combining DKT plate element with	
	triangular plane stress element with rotational DOFs	
Specific parameters	-	
Unknowns	Six dofs (u,v,w-displacements and u,v,w rotations) are in	
	general required in each node.	
Approximation	See description of cct and trplanstrrot elements	
Integration	4 integration points necessary, use "NIP 4" in element record.	
CS properties	Cross section thickness is required.	
Loads	Body loads are supported. Boundary loads are supported (only surface loads).	
Output	On output, the shell force (s_f) , shell strain (s_s) , shell mo-	
	mentum (s_m) , and shell curvature (s_c) tensors in global	
	poperta with the following meaning:	
	ponents, with the following meaning.	
	$s_f = \{n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}\},\$	
	$s_s = \{\varepsilon_x, \varepsilon_y, \varepsilon_z, \gamma_{yz}, \gamma_{xz}, \gamma_{xy}\},\$	
	$s_m = \{m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}\},\$	
	$s_c = \{\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}\}$	
	where $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are membrane normal deformations,	
	$\gamma_{zy}, \gamma_{zx}, \gamma_{xy}$ are (out of plane and in plane) shear componets, $\kappa_{x}, \kappa_{y}, \kappa_{z}, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}$ are curvatures,	
	$n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}$ are integral forces (normal and shear forces), and $m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}$ are bending moments. Please note, for example, that bending moment m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along the y-axis and positive value causes tension in bottom layer.	
Nlgeo	0.	
Status	-	

Table 24: tr_shell02 element summary

Keyword	quad1mindlin	
Description	Quadrilateral, bilinear, four-node Mindlin plate	
Specific parameters	$\begin{bmatrix} \text{NIP } \#(\text{in}) \end{bmatrix}$	
Unknowns	Three dofs (w-displacement, u and v - rotation) are required	
	in each node.	
Approximation	Linear for all unknowns.	
Integration	Default uses 4 integration points. No reduced integration is	
	used, as it causes numerical problems.	
Features	Layered cross section support.	
CS properties	Cross section thickness is required.	
Loads	Dead weight loads, and edge loads are supported.	
Output	On output, the generalized shell strain/force momentum	
	vectors in global coordinate system are printed, with the	
	following meaning:	
	$s_{\varepsilon} = \{\varepsilon_x, \varepsilon_y, \varepsilon_{xz}, \kappa_x, \kappa_y, \kappa_{xy}, \gamma_{xz}, \gamma_{yz}\},\$	
	$s_{\sigma} = \{n_x, n_y, n_{xy}, m_x, m_y, m_z, m_{xy}, q_{xz}, q_{yz}\}$	
	where $\varepsilon_x, \varepsilon_y, \varepsilon_{xy}$ are membrane in plane normal deforma-	
	tions, γ_{zx}, γ_{xz} are (out of plane and in plane) shear com-	
	ponets, $\kappa_x, \kappa_y, \kappa_{xy}$ are curvatures, $n_x, n_y, n_{xy}, q_{xz}, q_{yz}$ are	
	integral forces (normal and shear forces), and m_x, m_y, m_{xy}	
	are bending moments. Please note, for example, that bend-	
	ing moment m_x is defined as $m_x = \int \sigma_x z dz$, so it acts along	
	the y-axis and positive value causes tension in bottom layer.	
Nlgeo	0.	
Reference		
Status	Experimental	

Table 25:	quad1mindlin	element	summary
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Keyword	tr2shell7
Description	Triangular, quadratic, six-node shell with 7 dofs/node
Specific parameters	$[\texttt{NIP} \ \#_{(in)}]$
Unknowns	Seven dofs (displacement in u, v and w-direction; change
	in director field in u, v and w-direction; and inhomgenous
	thickness stretch) are required in each node.
Approximation	Quadratic for all unknowns.
Integration	Default uses 6 integration points in the midsurface plane.
	Number of integration points in the thickness direction is
	determined by the Layered cross section.
Features	Layered cross section support.
CS properties	This element must be used with a Layered cross section.
Loads	Edge loads, constant pressure loads and surface loads are supported.
Nlgeo	Not applicable. The implementation is for large deforma-
-	tions and hence geometrical nonlinearities will always be
	present, regardless the value of Nlgeo.
Reference	[3]
Status	Experimental

Table 26: tr2shell7 element summary

Keyword	mitc4shell	
Description	Quadrilateral, bilinear, four-node shell element using the	
	MITC technique.	
Specific parameters	$[\texttt{NIP} \ \#_{(in)}] \ [\texttt{NIPZ} \ \#_{(in)}] \ [\texttt{directorType} \ \#_{(in)}]$	
Parameters	NIP: allows to set the number of integration points in local	
	x-y plane (default 4).	
	NIPZ: allows to set the number of integration points in local	
	z-direction (default 2).	
	directorType: allows to set director vectors. Director	
	vectors can be set as normal to the plane (directorlype	
	= 0, default), or calculated for each node as an average of	
	-1) or can be specified at crosssection (directorType	
	= 1), or can be specified at crosssection (directorrype) =2).	
Unknowns	Six dofs (u.v.w-displacements and u.v.w rotations) are in	
••	general required in each node. Note, that although element	
	requires generally six DOFs per node, no stiffness to local	
	rotation along z-axis (rotation around director vector) is	
	supplied.	
Approximation	Linear approximation of displacements and rotations.	
Integration	Integration of all terms using Gauss integration formula in 8	
D	points (default) or specified using NIP and NIPZ parameters.	
Features	Variable cross section support.	
CS properties	Cross section thickness is required (measured along direc-	
	tor vector). Director vectors components may be specified [directory $\#_{\alpha}$][directory $\#_{\alpha}$][directory $\#_{\alpha}$] in ease	
	of directorType 2	
Loads	Body and boundary loads are supported.	
Output	On output, the shell force (s_f) , shell momentum (s_m) , shell	
-	strain (s_s) , shell curvature (s_c) , strain (ε) , and stress (σ)	
	tensors in global coordinate system are printed as vector	
	form with 6 components, with the following meaning:	
	$s_f = \{n_x, n_y, n_z, v_{yz}, v_{xz}, v_{xy}\},\$	
	$s_m = \{m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}\},\$	
	$s_{c} = \{\varepsilon_{m}, \varepsilon_{n}, \varepsilon_{n}, \varepsilon_{n}, \gamma_{mz}, \gamma_{mz}, \gamma_{mz}\},\$	
	$S_{x} = \{\kappa_{x}, \kappa_{y}, \kappa_{y}, \kappa_{y}, \kappa_{y}, \kappa_{y}\}$	
	$S_c = \{n_x, n_y, n_z, n_{yz}, n_{xz}, n_{xy}\}$	
	$z = \{z_x, z_y, z_z, \gamma_{yz}, \gamma_{zx}, \gamma_{xy}\},\$	
	$\sigma = \{\sigma_x, \sigma_y, \sigma_z, \sigma_{yz}, \sigma_{xz}, \sigma_{xy}\}.$	
	where $n_{\tau}, n_{\eta}, n_{\tau}, v_{\eta\tau}, v_{\tau\tau}, v_{\tau\eta}$ are integral forces (normal and	
	shear forces), and $m_x, m_y, m_z, m_{yz}, m_{xz}, m_{xy}$ are bending	
	moments, $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are membrane normal deformations,	
	$\gamma_{zy}, \gamma_{zx}, \gamma_{xy}$ are (out of plane and in plane) shear componets,	
	$\kappa_x, \kappa_y, \kappa_z, \kappa_{yz}, \kappa_{xz}, \kappa_{xy}$ are curvatures. Please note, for ex-	
	ample, the bending moment m_x is defined as $m_x = \int \sigma_x z dz$,	
	so it acts along the y-axis and positive value causes tension	
	In bottom layer (positive z-coordinate). The shell force (s_f) , shell momentum (a_i) shell strain (a_i) and shell surresture	
	(s_m) , she strain (s_m) , and she curvature	
	(thus are constant along the thickness) while the strain (ε)	
	and stress (σ) tensors are evaluated at each Gausspoint	
Nlgeo		
Status	-	

Table 27: mitc4shell element summary

Keyword	quad1plateSubsoil
Description	Quadrilateral, bilinear, four-node sub-soil plate element
Specific parameters	
Unknowns	One dof (w-displacement) is required in each node.
Approximation	Linear for transwersal displacement.
Integration	4 integration points.
Loads	Surface load support.
Note	Requires material model with 2dPlateSubSoil mode support.
Reference	[2]

Table 28: quad1platesubsoil element summary

Keyword	tria1platesubsoil
Description	Tringular, three-node sub-soil plate element with linear
	interpolation
Specific parameters	
Unknowns	One dof (w-displacement) is required in each node.
Approximation	Linear for transwersal displacement.
Integration	1 integration points.
Loads	Surface load support.
Note	Requires material model with 2dPlateSubSoil mode support.
Reference	[2]

Table 29: tria1plate
subsoil element summary $% \left({{{\left({{{{\bf{n}}}} \right)}_{{{\bf{n}}}}}} \right)$

2.7 Axisymmetric Elements

Implementation relies on elements located exclusively in x, y plane. The coordinate x corresponds to radius, y is the axis of rotation. Approximation of displacement functions u, v is carried out on a particular finite element. Nonzero strains read

$$\varepsilon_x = \varepsilon_r \quad = \quad \frac{\partial u}{\partial x} \tag{1}$$

$$\varepsilon_y = \varepsilon_z = \frac{\partial v}{\partial y}$$
 (2)

$$\varepsilon_{\theta} = \frac{u}{r} \tag{3}$$

$$\gamma_{xy} = \gamma_{rz} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$$
(4)

Stress components can be computed from elasticity matrix. Note that this matrix corresponds to a submatrix of the full 3D elasticity matrix.

$$\begin{cases} \sigma_x \\ \sigma_y \\ \sigma_\theta \\ \sigma_{xy} \end{cases} = \frac{E}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1-\nu & \nu & \nu & 0 \\ \nu & 1-\nu & \nu & 0 \\ \nu & \nu & 1-\nu & 0 \\ 0 & 0 & 0 & (1-2\nu)/2 \end{bmatrix} = \begin{cases} \varepsilon_x \\ \varepsilon_y \\ \varepsilon_\theta \\ \gamma_{xy} \end{cases}$$
(5)

In OOFEM, the strain vector is arranged as $\{\varepsilon_x, \varepsilon_y, \varepsilon_\theta, 0, 0, \gamma_{xy}\}^T$ and the stress vector $\{\sigma_x, \sigma_y, \sigma_\theta, 0, 0, \tau_{xy}\}^T$. Implementation assumes a segment of 1 rad.

2.7.1 Axisymm3d element

Implementation of triangular three-node finite element for axisymmetric continuum. Each node has 2 degrees of freedom. Node numbering and edge position is the same as in Fig. 7. The element features are summarized in Table 30.

Keyword	Axisymm3d
Description	Triangular axisymmetric linear element
Specific parameters	$[\texttt{NIP} \ \#_{(in)}] \ [\texttt{NIPfish} \ \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points (possible
	completions are 1 (default), 4 and 7 point integration rule).
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacement and geometry.
Integration	The integration can be altered using NIP paramter (default
	is 1 point integration).
Features	-
CS properties	-
Loads	Boundary and body loads are supported.
Nlgeo	0.
Status	-

Table 30: Axisymm3d element summary

2.7.2 Q4axisymm element

Implementation of quadratic isoparametric eight-node quadrilateral - finite element for axisymmetric 3d continuum. Each node has 2 degrees of freedom. The element features are summarized in Table 31.

Keyword	Q4axisymm
Description	Quadratic isoparametric eight-node quadrilateral for axisym-
	metric analysis
Specific parameters	$[\texttt{NIP} \ \#_{(in)}] \ [\texttt{NIPfish} \ \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points for inte-
	gration of terms corresponding to ε_x and ε_y strains (possible completions are 1, 4 (default), 9, and 16).
	NIPfish: allows to set the number of integration points
	for integration of remain terms (corresponding to ε_{θ} and
	γ_{rz}) (Supported values include 1 (default), 4, 9, and 16
	integration point formula).
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Quadratic approximation of displacement and geometry.
Integration	The integration of terms corresponding to ε_x and ε_y strains can be altered using NIP parameter (default is 4 point for- mula). The remaining terms (creesponding to ε_{θ} and γ_{rz}) are integrated by default using 1 point formula (see NIPfish parameter).
Features	-
CS properties	-
Loads	No boundary and body loads are supported.
Nlgeo	0.
Status	-

Table 31: Q4axisymm element summary

2.7.3 L4axisymm element

Implementation of isoparametric four-node quadrilateral axisymmetric finite element with linear interpolations of displacements u, v. Node numbering and edge position is the same as in Fig. 5. The element features are summarized in Table 32.

Keyword	L4axisymm
Description	Isoparametric four-node quadrilateral element for axisym-
	metric analysis
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points for inte-
	gration of terms corresponding to ε_x and ε_y strains (possible completions are 1, 4 (default), 9, and 16).
Unknowns	Two dofs (u-displacement, v-displacement) are required in each node.
Approximation	Linear approximation of displacement and geometry.
Integration	The integration of ε_x and ε_y strains can be altered using
	NIP parameter (possible completions are 1, 4 (default), 9
	or 16 point integration rule). The remaining strain compo-
	nents (ε_{θ} and γ_{rz}) are integrated using one point integration
	formula.
Features	-
CS properties	-
Loads	Boundary and body loads supported.
Nlgeo	0.
Status	-

Table 32: L4axisymm element summary

2.8 3d Continuum Elements

2.8.1 LSpace element

Implementation of Linear 3d eight - node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 33.



Figure 12: LSpace element (Node numbers in black, side numbers in blue, and surface numbers in red).

Keyword	lspace
Description	Linear isoparametric brick element
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points (possible
	completions are 1, 8 (default), or 27).
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Linear approximation of displacement and geometry.
Integration	Full integration of all strain components.
Features	Adaptivity support, Geometric nonlinearity support.
CS properties	-
Loads	-
Nlgeo	0,1,2.
Status	Reliable

Table 33: lspace element summary

2.8.2 LSpaceBB element

Implementation of 3d brick eight - node linear approximation element with selective integration of deviatoric and volumetric strain contributions (B-bar formulation) for incompressible problems. Features and description identical to conventional lspace element, see section 2.8.1.

2.8.3 QSpace element

Implementation of quadratic 3d 20-node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 34.



Figure 13: QSpace element.

Keyword	qspace
Description	Quadratic isoparametric brick element
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to set the number of integration points (possible
	completions are 1, 8 (default), or 27).
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Quadratic approximation of displacement and geometry.
Integration	Full integration of all strain components.
Features	-
CS properties	-
Loads	-
Nlgeo	0,1,2.
Status	Reliable

 Table 34: qspace element summary

2.8.4 LTRSpace element

Implementation of tetrahedra four-node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 35. Following node numbering convention is adopted (see also Fig. 14):

- Select a face that will contain the first three corners. The excluded corner will be the last one.
- Number these three corners in a counterclockwise sense when looking at the face from the excluded corner.

2.8.5 QTRSpace element

Implementation of tetrahedra ten-node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 36. Following node numbering convention is adopted (see also Fig. 15):

2.8.6 LWedge element

Implementation of wedge six-node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 37. Following node numbering convention is adopted (see also Fig. 16):



Figure 14: LTRSpace element. Definition and node numbering convention.

Keyword	LTRSpace
Description	Linear tetrahedra element
Specific parameters	-
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Linear approximation of displacements and geometry using
	linear volume coordinates.
Integration	Full integration of all strain components using four point
	Gauss integration formula.
Features	Adaptivity support, Geometric nonlinearity support.
CS properties	-
Loads	Surface and Edge loadings supported.
Nlgeo	0,1,2.
Status	Reliable

Table 35: LTRSpace element summary

2.8.7 QWedge element

Implementation of wedge fifteen-node finite element. Each node has 3 degrees of freedom. The element features are summarized in Table 38. Following node numbering convention is adopted (see also Fig. 17):



Figure 15: QTRSpace element. Definition and node numbering convention.

Keyword	QTRSpace
Description	3D tetrahedra element with quadratic interpolation
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to alter the default integration formula (possible
	completions are $1, 4$ (default), $5, 11, 15, 24$, and 45 point
	intergation formulas).
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Quadratic approximation of displacements and geometry
	using linear volume coordinates.
Integration	Full integration of all strain components using four point
	Gauss integration formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0,1,2.
Status	Reliable

Table 36: QTRSpace element summary



Figure 16: LWedge element. Node numbering convention in black, edge numbering in blue and face numbering in red.



Figure 17: QWedge element. Node numbering convention in black, edge numbering in blue and face numbering in red.

Keyword	I.Wedge
Description	3D wodge six node finite element with linear interpolation
Description	5D wedge six-node innite element with inlear interpolation
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to alter the default integration formula (pos-
	sible completions are 2 (default) and 9 point integration
	formulas).
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Full integration of all strain components using four point
	Gauss integration formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0,1,2.
Status	Reliable

Table 37: LWedge element summary

Keyword	QWedge
Description	3D wedge six-node finite element with quadratic interpola-
	tion
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to alter the default integration formula (pos-
	sible completions are 2 (default) and 9 point integration
	formulas).
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Quadratic approximation of displacements and geometry.
Integration	Full integration of all strain components using four point
	Gauss integration formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0,1,2.
Status	Reliable

Table 38: QWedge element summary

2.9 Interface elements

Interface elements represents an interaction between points, edges or surfaces. They are used to model debonding between surfaces or more general fracture processes through the use of cohesive zone (cz) models. They can also be used to model contact between elements. Specific interface material models needs to be used - consult the *matlibmanual* for supported models.

Ordering convention: All inerface elements have *plus*-side and a *minus*-side and all nodes should first be specified for the minus-side and then the plus-side. The normal to the interface is defined to point from the minus-side to the-plus side. Direction of normal vector on an element specifies normal stress/cohesion across the element. It is assumed that normal jump, normal traction are at the first position of corresponding vectors. Stiffness matrix in local coordinates has always on position 1,1 normal stiffness and then shear stiffness.

2.9.1 IntElPoint, Interface1d elements

Implementation of one dimensional (slip) interface element. This element connects two separate nodes and the interaction is governed by a one-dimensional slip law. This law determines the force acting between the nodes as a function on their relative displacement in the slip direction. The element can be used in 1D, 2D, and 3D (default) and its features are summarized in Table 39.

Keyword	IntElPoint, Interface1d (deprecated)
Description	One dimensional (slip) interface element
Specific parameters	$[\texttt{refnode} \ \#_{(in)}] \ [\texttt{normal} \ \#_{(ra)}]$
Parameters	refnode: determines the reference node, which is used to
	specify a reference direction (the direction vector is obtained
	by subtracting the coordinates of the first node from the reference node).
	normal: The reference direction can be directly specified
	by the optional parameter normal. Although both refnode
	and normal are optional, at least one of them must be
	specified.
Unknowns	One, two, or three DOFs (u-displacement, v-displacement,
	w-displacement) are required in each node, according to
	element mode (determined from domain type).
Approximation	-
Integration	-
Features	-
CS properties	-
Loads	-
Nlgeo	0
Status	Reliable
Note	Element requires material model with _1dInterface support.

 Table 39: IntElPoint element summary

2.9.2 IntElLine1, Interface2dlin elements

Implementation of a two dimensional line element with a linear approximation of the displacement jump. The element can be used to tie together two element edges and is defined by four nodes - two on each edge. Note that, the nodes along the interface are doubled, each couple with identical coordinates. Nodes on the negative side are numbered first, followed by nodes on the positive part. Requires material model with _2dInterface support. The element features are summarized in Table ??.



Figure 18: Interface2dlin element with linear interpolation. Definition and node numbering convention

Keyword	IntElLine1, Interface2dlin(deprecated)
Description	2D interface element with linear approximation
Specific parameters	$[axisymmode \#_0]$
Parameters	axisymmode: Flag controlling axisymmetric mode (integra-
	tion over unit circumferential angle).
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Full integration of all strain components using two point
	integration formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0
Status	Reliable
Note	Element requires material model with _2dInterface support.

Table 40: IntElLine1 element summary

2.9.3 IntElLine2, Interface2dquad elements

Implementation of a two dimensional interface element with quadratic approximation of displacement field. Can be used to glue together two elements with quadratic displacement approximation along the shared edge. Note, that the nodes along the interface are doubled, each couple with identical coordinates. Nodes on the negative side are numbered first, followed by nodes on the positive part. Requires material model with _2dInterface support. The element features are summarized in Table **??**.

2.9.4 IntElSurfTr1, Interface3dtrlin elements

Implementation of a three dimensional interface element with linear approximation of displacement field. Can be used to glue together two elements with linear displacement approximation along the shared triangular surface. Note, that the nodes along the interface are doubled, each couple with identical coordinates. Nodes on the negative surface are numbered first, followed by nodes on the positive part. The numbering of surface nodes on positive surface (+) determines the positive normal (right hand rule). Requires material model with _3dInterface support. The element features are summarized in Table 42.



Figure 19: Interface2dquad element with quadratic interpolation. Definition and node numbering convention

Keyword	IntElLine2, Interface2dquad (deprecated)
Description	2D interface element with quadratic approximation
Specific parameters	[axisymmode #0]
Parameters	axisymmode: Flag controlling axisymmetric mode (integra-
	tion over unit circumferential angle).
Unknowns	Two dofs (u-displacement, v-displacement) are required in
	each node.
Approximation	Quadratic approximation of displacements and geometry.
Integration	Full integration of all strain components using four point
	integration formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0
Status	Reliable
Note	Element requires material model with _2dInterface support.

Table 41: IntElLine2 element summary

Keyword	IntElSurfTr1, Interface3dtrlin (deprecated)
Description	3D interface element with linear approximation
Specific parameters	-
Unknowns	Three dofs (u-displacement, v-displacement, w-
	displacement) are required in each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Full integration of all components using one point integration
	formula.
Features	-
CS properties	-
Loads	-
Nlgeo	0
Status	Reliable
Note	Element requires material model with _3dInterface support.

Table 42: IntElSurfTr1 element summary



Figure 20: Interface3dtrlin element with linear interpolation. Definition and node numbering convention

2.10 Free warping analysis elements

2.10.1 TrWarp

Implements 2D linear triangular three-node finite element for FreeWarping analysis. Each node has 1 degree of freedom. The node numbering is anti-clockwise. The element features are summarized in Table 43.

Keyword	TrWarp
Description	2D linear triangular warping element
Specific parameters	-
Unknowns	One dof (the value of deplanation function) is required in
	each node.
Approximation	Linear approximation of displacements and geometry.
Integration	Integration using one point gauss integration formula.
Features	This type of element is supported in FreeWarping analysis
	only.
CS properties	Only warpingCS is supported.
Loads	Edge loads corresponding to free warping problem are gener-
	ated automatically. Additional edge loads are not supported.
Nlgeo	0.
Status	-
Note	Test case: sm/freewarpingtest2.in

Table 43: TrWarp element summary

2.11 XFEM elements

XFEM elements allow simulations where the unknown fields are enriched through the partition of unity concept. Two elements are currently available for 2D XFEM simulations: TrPlaneStress2dXFEM (subclass of TrPlaneStress2d) and PlaneStress2dXfem (subclass of PlaneStress2d).

2.11.1 TrPlaneStress2dXFEM element

Keyword	TrPlaneStress2dXFEM
Description	Two dimensional 3-node triangular XFEM element
Specific parameters	$[\texttt{czmaterial} \#_{(in)}] [\texttt{nipcz} \#_{(in)}] [\texttt{useplanestrain} \#_{(in)}]$
Parameters	czmaterial: Interface material for the cohesive zone. (If
	no material is specified, traction free crack surfaces are assumed.)
	nipcz : Number of integration points used on each segment of the cohesive zone.
	useplanestrain : If plane strain or plane stress should be assumed. 0 implies plane stress and 1 implies plane strain.
Unknowns	Two continuous (standard) DOFs (u-displacement, v- displacement) and a variable number of enriched DOFs (can be continuous or discontinuous).
Approximation	-
Integration	Elements cut by an XFEM interface are divided into subtri- angles.
Features	-
CS properties	-
Loads	-
Nlgeo	-
Status	-
Note	Test case: sm/xFemCrackVal.in

Table 44: TrPlaneStress2dXFEM element summary

2.11.2 PlaneStress2dXfem element

Keyword	PlaneStress2dXfem
Description	Two dimensional 4-node quad XFEM element
Specific parameters	$[\texttt{czmaterial} \ \#_{(in)}] \ [\texttt{nipcz} \ \#_{(in)}] [\texttt{useplanestrain} \ \#_{(in)}]$
Parameters	czmaterial: Interface material for the cohesive zone. (If
	no material is specified, traction free crack surfaces are
	assumed.)
	nipcz: Number of integration points used on each segment
	of the cohesive zone.
	useplanestrain: If plane strain or plane stress should be
	assumed. 0 implies plane stress and 1 implies plane strain.
Unknowns	Two continuous (standard) DOFs (u-displacement, v-
	displacement) and a variable number of enriched DOFs
	(can be continuous or discontinuous).
Approximation	-
Integration	Elements cut by an XFEM interface are divided into subtri-
	angles.
Features	-
CS properties	-
Loads	-
Nlgeo	-
Status	-
Note	Test cases: sm/xFemCrackValBranch.in,
	sm/xfemCohesiveZone1.in, benchmark/xfem01.in

Table 45: PlaneStress2dXfem element summary

2.12 Iso Geometric Analysis based (IGA) elements

The following record describes the common part of IGA element record:

```
*IGAElement (num\#)_{(in)}
mat \#_{(in)} crossSect \#_{(in)} nodes \#_{(ia)}
knotvectoru \#_{(ra)} knotvectorv \#_{(ra)} knotvectorw \#_{(ra)}
[knotmultiplicityu \#_{(ia)}]
[knotmultiplicityw \#_{(ia)}]
degree \#_{(ia)} nip \#_{(ia)}
\langle[partitions \#_{(ia)}]\rangle \langle[remote \#_{()}]\rangle
```

The knotvectoru, knotvectorv, and knotvectorw parameters specify knot vectors in individual parametric directions, considering only distinct knots. Open knot vector is always assumed, so the multiplicity of the first and last knot should be equal to p + 1, where p is polynomial degree in corresponding direction (determined by degree parameter, see further).

The knot multiplicity can be set using optional parameters knotmultiplicityu, knotmultiplicityv, and knotmultiplicityw. By default, the open knot vector is assumed and multiplicity of internal knots is assumed to be equal to one. Note, that total number of knots in particular direction (including multiplicity) must be equal to number of control points in this direction increased by degree in this direction plus 1.

The degree of approximation for each parametric direction is determined from degree array, dimension of which is equal to number of spatial dimensions of the problem.

In case of elements with BSpline or Nurbs interpolation, the nodes forming the rectangular array of control points of the element are ordered in a such way, that u-index is changing most quickly, and w-index (or v-index in case of 2d problems) most slowly. In case of elements with T-spline interpolation, the nodes forming the T-mesh of the element are ordered arbitrarily.

The supported ***IGAElement** values are following:

 ${\bf Keyword: bsplineplanestresselement}$

Parameters: None.

Keyword: nurbsplanestresselement

Parameters: None.

 $\mathbf{Keyword}:$ nurbs3delement

Parameters: None.

Keyword: tsplineplanestresselement

Parameters: localindexknotvectoru $\#_{(in)}$ localindexknotvectorv $\#_{(in)}$ localindexknotvectorw $\#_{(in)}$. The parameters localindexknotvectoru, localindexknotvectorv,

and localindexknotvectorw defined by the indices to global knot vectors (given by knotvectoru, knotvectorv, and knotvectorw parameters) specify the local knot vectors for each control point of T-mesh (node) in the same order as the nodes have been specified for the element. The local knot vector in a particular direction has p + 2 entries, where the p is the polynomial degree in that direction.

2.13 Special elements

2.13.1 LumpedMass element

This element, defined by a single node, allows to introduce additional concentrated mass and/or rotational inertias in a node. A different mass and rotary inertia may be assigned to each coordinate direction. At present, individual mass/inertia components can be specified for every degree of freedom of element node. Only displacement and rotational degrees of freedom are considered. The element features are summarized in Table 46.

Keyword	LumpedMass
Description	Lumped mass element
Specific parameters	components $\#_{(ra)}$
Parameters	components: allows to specify additional concentrated
	mass components (Force*Time ² /Length) and rotary inertias
	(Force*Length*Time ²) about the nodal coordinate axes.
	dofs: dofs to which the components apply.
Unknowns	As specified by dofs.
Approximation	-
Integration	-
Features	-
CS properties	-
Loads	-
Status	Reliable

Table 46: LumpedMass element summary

2.13.2 Spring element

This element represent longitudial or torsional spring element. It is defined by two nodes, orientation and a spring constant. The spring element has no mass associated, the mass can be added using LumpedMass element. The spring is linear and works the same way in tension or in compression. The element features are summarized in Table 47.

Keyword	Spring
Description	Spring element
Specific parameters	mode $\#_{(in)} \ k \ \#_{(rn)} \ [m \ \#_{(rn)}]$ orientation $\#_{(ra)}$
Parameters	mode: defines the type of spring element (see Table 48).
	k: determines the spring constant, corresponding
	units are [Force/Length] for longitudinal spring and
	[Force*Length/Radian] for torsional spring.
	orientation: defines orientation vector of spring element
	(of size 3) - for longitudinal spring it defines the direction of
	spring, for torsional spring it defines the axis of rotation.
	m: determines optional mass of the element, zero value
	assumed by default.
Note	the spring element nodes doesn't need to be coincident, but
	the spring orientation is always determined by orientation
	vector.

Table 47: Spring element summary

 1D spring element along x-axis, requires D_u DOF in each node, orientation vector is {1,0,0} 2D spring element in xy plane, requires D_u and D_v DOFs in each node (orientation vector should be in xy plane) 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 	mode	description
 requires D_u DOF in each node, orientation vector is {1,0,0} 2D spring element in xy plane, requires D_u and D_v DOFs in each node (orientation vector should be in xy plane) 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 	0	1D spring element along x-axis,
 2D spring element in xy plane, requires D_u and D_v DOFs in each node (orientation vector should be in xy plane) 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		requires D_u DOF in each node, orientation vector is $\{1,0,0\}$
 requires D_u and D_v DOFs in each node (orientation vector should be in xy plane) 2 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 3 2D torsional spring element in xz plane, requires R_v DOFs in each node 4 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 5 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 	1	2D spring element in xy plane,
 (orientation vector should be in xy plane) 2 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 3 2D torsional spring element in xz plane, requires R_v DOFs in each node 4 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 5 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		requires D_u and D_v DOFs in each node
 2 2D spring element in xz plane, requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 3 2D torsional spring element in xz plane, requires R_v DOFs in each node 4 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 5 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		(orientation vector should be in xy plane)
 requires D_u and D_w DOFs in each node (orientation vector should be in xz plane) 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 	2	2D spring element in xz plane,
 (orientation vector should be in xz plane) 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		requires D _u and D _w DOFs in each node
 2D torsional spring element in xz plane, requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		(orientation vector should be in xz plane)
 requires R_v DOFs in each node 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 	3	2D torsional spring element in xz plane,
 3D spring element in space, requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node 		requires R_v DOFs in each node
5 requires D_u, D_v, and D_w DOFs in each node 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node	4	3D spring element in space,
5 3D torsional spring in space, requires R_u, R_v, and R_w DOFs in each node		requires D ₋ u, D ₋ v, and D ₋ w DOFs in each node
requires Ru , Rv , and Rw DOFs in each node	5	3D torsional spring in space,
		requires R_u, R_v, and R_w DOFs in each node

Table 48: Supported spring element modes

nlgeo	strain tensor
0 (default)	Small-strain tensor
1	Green-Lagrange strain tensor
2	Deformation gradient

Table 49: Nonlinear geometry modes

2.14 Geometric nonlinear analysis

To take int account geometric nonlinearity for a specific element, the keyword nlgeo must be specified. The nlgeo parameter defines which formulation of the momentum balance is solved and what deformation measure that is computed and sent to the constitutive models (see Table 49). If nlgeo=1, then the momentum balance is set up in the reference configuration in terms of the First Piola-Kirchhoff stress tensor \mathbf{P} and the deformation tensor \mathbf{F} as energy conjugates. This is also referred to a Total Lagrangian formulation. The balance equation in weak form reads

$$\int_{\Omega} \delta \mathbf{F} : \mathbf{P} d\Omega = \int_{\Gamma} \delta \mathbf{x} \cdot \mathbf{t}_{P} d\Gamma + \int_{\partial \Omega} \delta \mathbf{x} \cdot \mathbf{b}_{P} d\Omega$$
(6)

This equation can be rewritten in terms of the displacement ${\bf u}$ and the displacement gradient ${\bf H}$

$$\int_{\Omega} \delta \mathbf{H} : \mathbf{P} d\Omega = \int_{\Gamma} \delta \mathbf{u} \cdot \mathbf{t}_{P} d\Gamma + \int_{\partial \Omega} \delta \mathbf{u} \cdot \mathbf{b}_{P} d\Omega$$
(7)

This equation is nearly identical to the one for small strains except that another stress measure is used and we have the virtual displacement gradient instead of the virtual strains.

The corresponding FE-formulation is obtained as

$$\int_{\Omega} \mathbf{B}_{H}^{\mathrm{T}} \cdot \mathbf{P} \mathrm{d}\Omega = \int_{\Gamma} \mathbf{N}^{\mathrm{T}} \cdot \mathbf{t}_{P} \mathrm{d}\Gamma + \int_{\partial\Omega} \delta \mathbf{N}^{\mathrm{T}} \cdot \mathbf{b}_{P} \mathrm{d}\Omega$$
(8)

with the tangent stiffness

$$\mathbf{K}_{\mathrm{T}} = \int_{\Omega} \mathbf{B}_{H}^{\mathrm{T}} \cdot \frac{\partial \mathbf{P}}{\partial \mathbf{F}} \cdot \mathbf{B}_{H} \mathrm{d}\Omega \tag{9}$$

Thus, for an element to support large deformations (in addition to small deformation) it needs only to implement the \mathbf{B}_H matrix. Similar to the regular \mathbf{B} matrix, which gives the strains in Voigt form when multiplied with the solution vector \mathbf{a} , \mathbf{B}_H should give the displcement gradient in Voigt form with 9 components for a full 3D state.

3 Elements for Transport problems (TM Module)

3.1 2D Elements

3.1.1 Tr1ht element

Implements the linear triangular finite element for heat transfer problems. Each node has 1 degree of freedom. The cross section thickness property is requested form cross section model. The node numbering is anti-clockwise. The element features are summarized in Table 50.



Figure 21: Tr1ht element - node and side numbering.

Keyword	Tr1ht
Description	triangular finite element with linear approximation for heat
	transfer problems
Specific parameters	-
Unknowns	Single dof (T_f - temperature) is required in each node.
Approximation	Linear approximation of temperature.
Integration	Integration using one point gauss integration formula.
Loads	Body loads are supported. Boundary loads are supported and are computed using numerical integration. The side numbering is following. Each i-th element side begins in i-th element node and ends on next element node (i+1-th node or 1-st node, in the case of side number 3). The local positive edge x-axis coincides with side direction, the positive local edge y-axis is rotated 90 degrees anti-clockwise (see fig. (21)).
Features CS properties Status	-

Table 50: Tr1ht element summary

3.1.2 Tr1mt element

Isoparametric triangular finite element with linear approximation of moisture. Other features are the same as for Tr1ht in Section 3.1.1.

3.1.3 Tr1hmt element

Isoparametric triangular finite element with linear approximations of temperature and moisture. Other features are the same as for Tr1ht in Section 3.1.1.

3.1.4 Quad1ht element

Represents isoparametric four-node quadrilateral finite element for heat transfer problems. Each node has 1 degree of freedom. Problem should be defined in x,y plane. The cross section thickness property is requested form cross section model. The nodes should be numbered anti-clockwise (positive rotation around z-axis). The element features are summarized in Table 51.



Figure 22: Quad1ht element. Node numbering, Side numbering and definition of local edge c.s.(a).

Keyword	Quad1ht
Description	Isoparametric four-node quadrilateral linear interpolation
	element for heat transfer problems
Specific parameters	$[\texttt{NIP} \ \#_{(in)}]$
Parameters	NIP: allows to change the default number of integration point used.
Unknowns	Single dof (T_f - temperature) is required in each node.
Approximation	Linear approximation of temperature.
Integration	Integration using gauss integration formula in 4 (the de-
	fault), 9, or 16 integration points. The default number of
	integration point used can be overloaded using NIP parame-
	ter.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side num-
	bering is following. Each i-th element side begins in i-th
	element node and ends on next element node $(1+1-th node)$
	or 1-st flode, in the case of side number 4). The local posi-
	local adge y axis is retated 00 degrees anti algebraice (see
	for (22)
Footurog	lig. $(22))$.
CS properties	-
Status	-
Status	

Table 51: Quad1ht element summary

3.1.5 Quad1mt element

Isoparametric four-node quadrilateral finite element. Other features are the same as for Quad1ht in Section 3.1.4.

3.1.6 Quad1hmt element

Represents isoparametric four-node quadrilateral finite element for heat and mass (one constituent) transfer problems. Two dofs (T_f - temperature and C_1 - concentration) are required in each node. Linear approximation of temperature and mass concentration. Other features are similar to Quad1 element, see section 3.1.4.

3.2 Axisymmetric Elements

3.2.1 Quadaxisym1ht element

Isoparametric four-node quadrilateral finite element for axisymmetric heat transfer problems. The element description is similar to Quad1 element, see section 3.1.4.

3.2.2 Traxisym1ht element

Linear triangular finite element for axisymmetric heat transfer problems. The element description is similar to Tr1ht element, see section 3.1.1.

3.3 3D Elements

3.3.1 Tetrah1ht - tetrahedral 3D element

Represents isoparametric four-node tetrahedral element. Each node has 1 degree of freedom. The same numbering convection is adopted as in mechanics, see Fig. 14. The element features are summarized in Table 52.

Keyword	Tetrah1ht
Description	Isoparametric, four-node tetrahedral element with linear
	approximation for heat transfer problems
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to change the default number of integration
	point used.
Unknowns	Single dof (T_f - temperature) is required in each node.
Approximation	Linear approximation of temperature.
Integration	Integration using gauss integration formula in 1 (the default),
	or 4 integration points. The default number of integration
	point used can be overloaded using NIP parameter.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side and
	surface numbering is shown in Fig. 14.
Features	-
CS properties	-
Status	

Table 52: Tetrah1ht element summary

3.3.2 Brick1ht - hexahedral 3D element

Represents isoparametric eight-node brick/hexahedron finite element for heat transfer problems. Each node has 1 degree of freedom. The element features are summarized in Table 53.



Figure 23: Brick1ht element. Node numbers are in black, side numbers are in blue, and surface numbers are in red.

Keyword	Brick1ht
Description	Isoparametric, hexahedral 3D element with linear approxi-
	mation for heat transfer problems
Specific parameters	$[\texttt{NIP } \#_{(in)}]$
Parameters	NIP: allows to change the default number of integration
	point used.
Unknowns	Single dof (T_f - temperature) is required in each node.
Approximation	Linear approximation of temperature.
Integration	Integration using gauss integration formula in 8 (the default),
	or 27 integration points. The default number of integration
	point used can be overloaded using NIP parameter.
Loads	Body loads are supported. Boundary loads are supported
	and computed using numerical integration. The side and
	surface numbering is shown in fig. (23)).
Features	-
CS properties	-
Status	

Table 53: Brick1ht element summary

3.3.3 Brick1hmt - hexahedral 3D element

Represents isoparametric eight-node quadrilateral finite element for heat and mass (one constituent) transfer problems. Two dofs (T_f - temperature and C_1 - concentration) are required in each node. Linear approximation of temperature and mass concentration. Other features are similar to Brick1 element, see section 3.3.2.

3.3.4 QBrick1ht - quadratic hexahedral 3D element

Implementation of quadratic 3d 20-node finite element. Each node has 1 degree of freedom. See section 2.8.3 for node numbering order and order of faces. The element features are summarized in Table 54.

77 1	
Keyword	QBrick1ht
Description	Isoparametric, hexahedral 3D element with quadratic ap-
	proximation for heat transfer problems
Specific parameters	$[NIP \#_{(in)}]$
Parameters	NIP: allows to change the default number of integration
	point used, possible values are 8, 27 (default) and 64.
Unknowns	Single dof (T_f - temperature) is required in each node.
Approximation	Quadratic approximation of temperature and geometry
Integration	Integration using gauss integration formula in 8, 27 (default),
	or 64 integration points. The default number of integration
	point used can be overloaded using NIP parameter.
Loads	-
Features	-
CS properties	-
Status	

Table 54: QBrick1ht element summary

3.3.5 QBrick1hmt - quadratic hexahedral 3D element

The same element as QBrick1ht for heat and mass (one constituent) transfer problems. Two dofs (T_f - temperature and C_1 - concentration) are required in each node. Linear approximation of temperature and

mass concentration. Other features are similar to QBrick1ht element, see section 3.3.4.

4 Elements for Fluid Dynamics problems (FM Module)

4.1 Stokes' Flow Elements

Stokes' flow elements neglect acceleration, and thus requires no additional stabilization.

4.1.1 Tr21Stokes element

Standard 6 node triangular element for stokes flow, with quadratic geometry, velocity and linear pressure. Both compressible and incompressible material behavior is supported (and also the seamless transition between the two). The element features are summarized in Table 55.

Keyword	Tr121Stokes
Description	Standard 6 node triangular element for stokes flow, with
	quadratic geometry, velocity and linear pressure
Specific parameters	-
Unknowns	Unknown pressure in nodes 1–3 with unknown velocity (V_u
	and V_v in all 6 nodes.
Approximation	Quadratic approximation of geometry and velocity, linear
	pressure approximation.
Integration	
Features	-
Status	Reliable

Table 55: Tr121Stokes element summary

4.1.2 Tet21Stokes element

Standard 10 node tetrahedral element for stokes flow, with quadratic geometry, velocity and linear pressure. The element features are summarized in Table 56.

Keyword	Tet21Stokes
Description	Standard 10 node tetrahedral element for stokes flow, with
	quadratic geometry, velocity and linear pressure
Specific parameters	-
Unknowns	Unknown pressure (P_f) in nodes 1–4, and unknown velocity
	(V_u, V_v, V_w) in all nodes.
Approximation	Quadratic approximation of geometry and velocity, linear
	pressure approximation.
Integration	
Features	-
Status	Untested

Table 56: Tet21Stokes element summary

4.1.3 Hexa21Stokes element

Standard 27 node hexahedral element for stokes flow, with quadratic geometry, velocity and linear pressure. The element features are summarized in Table 57.



Figure 24: Hexa21Stokes element. Node numbering and face numbering.

Keyword	Hexa21Stokes
Description	Standard 10 node tetrahedral element for stokes flow, with
	quadratic geometry, velocity and linear pressure
Specific parameters	-
Unknowns	Unknown pressure (P_f) in nodes 1–8, and unknown velocity
	(V_u, V_v, V_w) in all nodes.
Approximation	Quadratic approximation of geometry and velocity, linear
	pressure approximation.
Integration	
Features	-
Status	Untested

Table 57: Hexa21Stokes element summary

4.1.4 Tr1BubbleStokes element

So called "Mini" element in 2D. A 3 node triangular element for stokes flow, with linear geometry and pressure. Velocity is enriched by a bubble function. Should not be used with materials that have memory (which is uncommon for flow problems). The element features are summarized in Table 58.

Keyword	Tr1BubbleStokes
Description	So called "Mini" 2D element
Specific parameters	-
Unknowns	Unknown pressure (P_f) in all nodes, and unknown velocity
	(V ₋ u, V ₋ v) in all nodes and one internal dof manager.
Approximation	Linear geometry and pressure. Velocity is enriched by a
	bubble function.
Integration	
Features	-
Status	Untested

Table 58: Tr1BubbleStokes element summary

4.1.5 Tet1BubbleStokes element

So called "Mini" element in 3D. A 4 node tetrahedral element for stokes flow, with linear geometry and pressure. Velocity is enriched by a bubble function. Should not be used with materials that have memory (which is

uncommon for flow problems). The element features are summarized in Table 59.

Keyword	Tet1BubbleStokes
Description	So called "Mini" 3D element
Specific parameters	-
Unknowns	Unknown pressure (P_f) in all nodes, and unknown velocity
	(V _u , V _v) in all nodes and one internal dof manager.
Approximation	Linear geometry and pressure. Velocity is enriched by a
	bubble function.
Integration	
Features	-
Status	Untested

Table 59: Tet1BubbleStokes element summary

4.2 2D CBS Elements

4.2.1 Tr1CBS element

Represents the linear triangular finite element for transient incompressible flow analysis using cbs algorithm with equal order approximation of velocity and pressure fields. Each node has 3 degrees of freedoms (two components of velocity and pressure). The node numbering is anti-clockwise. The element features are summarized in Table 60.



Figure 25: Tr1CBS element. Node numbering, Side numbering and definition of local edge c.s.(a).

Keyword	Tr1CBS	
Description	linear triangular finite element for transient incompressible	
	flow analysis using cbs algorithm	
Specific parameters	$[\texttt{bsides } \#_{(ia)}] \ [\texttt{bcodes } \#_{(ia)}]$	
Parameters	Since the problem formulation requires to evaluate some	
	boundary terms, the element boundary edges should be	
	specified as well as the types of boundary conditions applied	
	at these boundary edges. The boundary edges (their num-	
	bers) are specified using bsides array. The type of bound-	
	ary condition(s) applied to corresponding boundary side	
	is determined by bcodes array. The available/supported	
	boundary codes are following: 1 for prescribed traction, 2	
	for prescribed normal velocity, 4 for prescribed tangential	
	velocity, and 8 for prescribed pressure. If the element side	
	is subjected to a combination of these fundamental types	
	boundary conditions, the corresponding code is obtained by	
	summing up the corresponding codes.	
Unknowns	Two velocity components (V ₋ u and V ₋ v) and pressure (P ₋ f)	
	are required in each node.	
Approximation	Equal order approximation of velocity and pressure fields.	
Integration	exact	
Features	Constant boundary tractions are supported ¹ . Body loads	
	representing the self-weight load are supported.	
Status	Untested	

Table 60: Tr1CBS element summary

4.3 2D SUPG/PSGP Elements

4.3.1 Tr1SUPG element

Represents the linear triangular finite element for transient incompressible flow analysis using SUPG/PSPG stabilization with equal order approximation of velocity and pressure fields. Each node has 3 degrees of freedoms (two components of velocity and pressure). The node numbering is anti-clockwise. The element features are summarized in Table 61.



Figure 26: Tr1SUPG element. Node numbering, Side numbering and definition of local edge c.s.(a).

Keyword	Tr1SUPG
Description	linear triangular finite element for transient incompressible
_	flow analysis using SUPG/PSPG algorithm
Specific parameters	$[\texttt{vof } \#_{(\texttt{rn})}] \; [\texttt{pvof } \#_{(\texttt{rn})}]$
Unknowns	Two velocity components (V_u and V_v) and pressure (P_f)
	are required in each node.
Approximation	Linear approximation of velocity and pressure fields.
Integration	exact
Loads	Constant boundary tractions are supported. Body loads representing the self-weight load are supported.
Multi-fluid analysis	The element has support for solving problems with two immiscible fluids in a fixed spatial domain. In the present implementation, a VOF and LevelSet tracking algorithms are used to track the position of interface. In case of VOF tracking, an initial VOF fraction (volume fraction of ref- erence fluid) can be specified using vof (default is zero). Element can also be marked as allways filled with reference fluid (some form of source) using parameter pvof which spec- ifies the permanent VOF value. In case of LevelSet tracking.
Status	the initial levelset is specified using reference polygon (see corresponding levelset record in oofem input manual). The material model should be of type Keyword : twofluidmat, that supports modelling of two immiscible fluids. Reliable

Table 61: 7	Ir1SUPG	element	summary
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4.3.2 Tr21SUPG element

Implementation of P2P1 Taylor Hood element for transient incompressible flow analysis using SUPG and LSIC stabilization. It consists of globally continuous, piecewise quadratic functions for approximation in velocity space and globally continuous, piecewise linear functions for approximation in pressure space. LBB condition is

satisfied. There are 3 degrees of freedom in vertices (two components of velocity and pressure), and 2 degrees of freedom in edge nodes (two components of velocity only). The node numbering is anti-clockwise, vertices are numbered first. The element features are summarized in Table 62.



Figure 27: Tr21SUPG element - node and side numbering.

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Table 62: Tr21SUPG element summary

4.3.3 Tr1SUPGAxi element

Represents the linear triangular finite element for transient incompressible flow analysis using SUPG/PSPG stabilization with equal order approximation of velocity and pressure fields in 2d-axisymmetric setting. Each node has 3 degrees of freedoms (two components of velocity and pressure). The y-axis is axis of ratational symmetry. The node numbering is anti-clockwise. The element features are summarized in Table 63.



Figure 28: Tr1SUPGAxi element. Node numbering, Side numbering and definition of local edge c.s.(a).

Keyword	Tr1SUPGAxi
Description	linear equal order approximation axisymmetric element
Specific parameters	$[\texttt{vof } \#_{(\texttt{rn})}][\texttt{pvof } \#_{(\texttt{rn})}]$
Unknowns	Two velocity components (V_u and V_v) and pressure (P_f)
	are required in each node.
Approximation	Linear approximation of velocity and pressure fields.
Integration	Gauss integration in seven point employed.
Loads	Constant boundary tractions are supported. Body loads
	representing the self-weight load are supported.
Multi-fluid analysis	The element has support for solving problems with two
	immiscible fluids in a fixed spatial domain. In the present
	implementation, a VOF tracking algorithm is used to track
	the position of interface. An initial VOF fraction (volume
	fraction of reference fluid) can be specified using vof (default
	is zero). Element can also be marked as always filled with
	reference fluid (some form of source) using parameter pvof
	which specifies the permanent VOF value. In this case, the
	material model should be of type Keyword : twofluidmat,
	that supports modelling of two immiscible fluids.
Status	

Table 63: Tr1SUPGAxi element summary

4.4 3D SUPG/PSGP Elements

4.4.1 Tet1_3D_SUPG element

Represents 3D linear pyramid element for transient incompressible flow analysis using SUPG/PSPG stabilization with equal order approximation of velocity and pressure fields. Each node has 3 degrees of freedoms (two components of velocity and pressure). The element features are summarized in Table 64.



Figure 29: Tet1_3D_SUPG element.

Keyword	TET1SUPG
Description	linear equal order approximation axisymmetric element
Specific parameters	$[\texttt{vof } \#_{(\mathrm{rn})}][\texttt{pvof } \#_{(\mathrm{rn})}]$
Unknowns	Three velocity components (V_u, V_v, and V_w) and pres-
	sure (P_f) are required in each node.
Approximation	Linear approximation of velocity and pressure fields.
Integration	exact
Loads	Constant boundary tractions are supported. Body loads
	representing the self-weight load are supported.
Multi-fluid analysis	The element has support for solving problems with two
	immiscible fluids in a fixed spatial domain. In the present
	implementation, a LevelSet tracking algorithm is used to
	track the position of interface. The material model should be
	of type Keyword : twofluidmat, that supports modelling
	of two immiscible fluids.
Status	
	· · ·

Table 64: TET1SUPG element summary

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